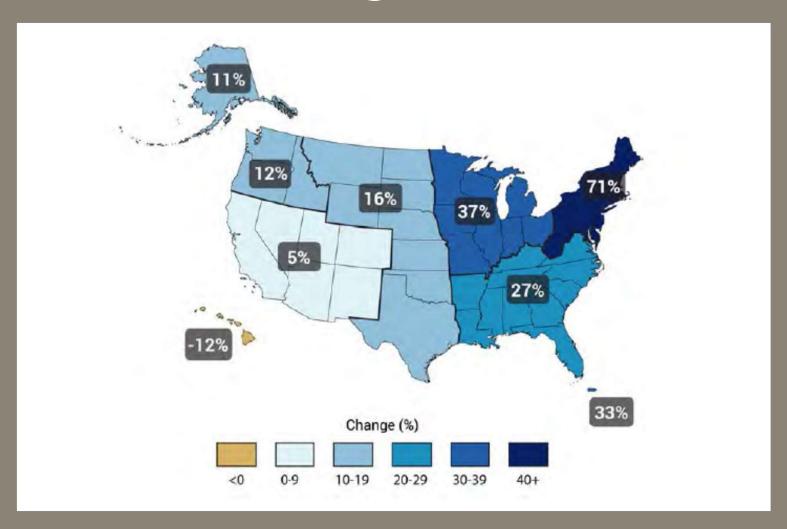


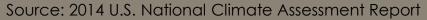
Presentation Overview

- 1 Cambridge CCVA
- 2 The Alewife Brook Area
- 3 Hydraulic Model Integration
- 4 Hydraulic Model Calibration and Validation
- **5** Potential Future Uses
- 6 Conclusions



1 Cambridge CCVA, Part 1

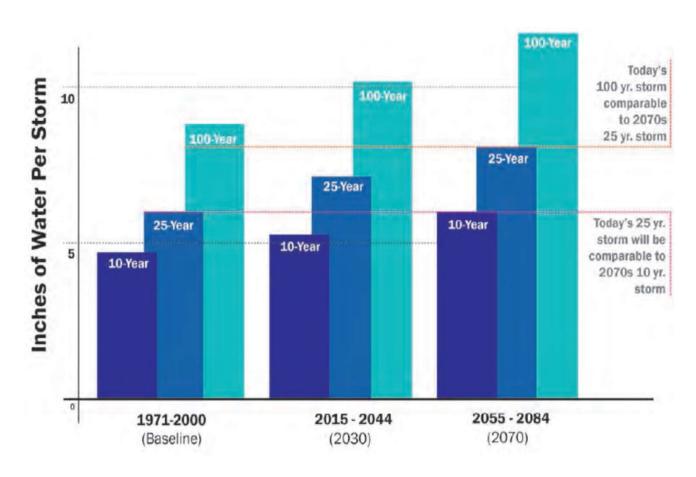






Cambridge CCVA, Part 1

Increase in Precipitation

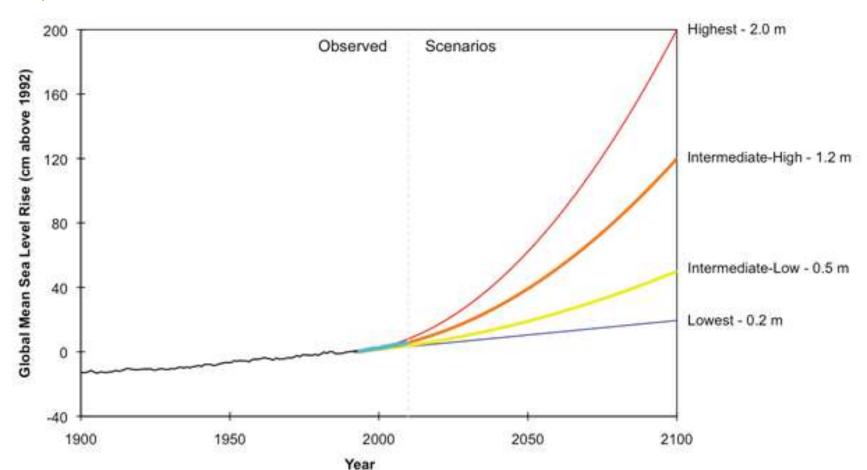


Source: 2015 Cambridge CCVA, Part 1



Cambridge CCVA, Part 1

SLR/SS



Source: NOAA (2012). Global Sea Level Rise Scenarios for the United States National Climate Assessment



Flood Modeling in the CCVA

Riverine Overbank Flooding from Precipitation

Captured using HEC-RAS model

Sewer System Flooding from Precipitation or River Backups

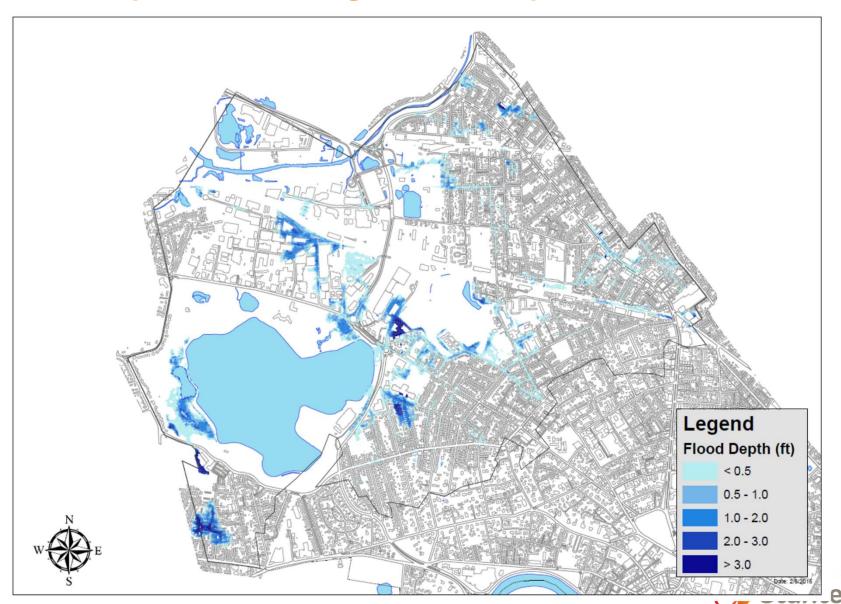
Captured Using City's Infoworks ICM Model

Riverine Overbank Flooding from SLR/SS events

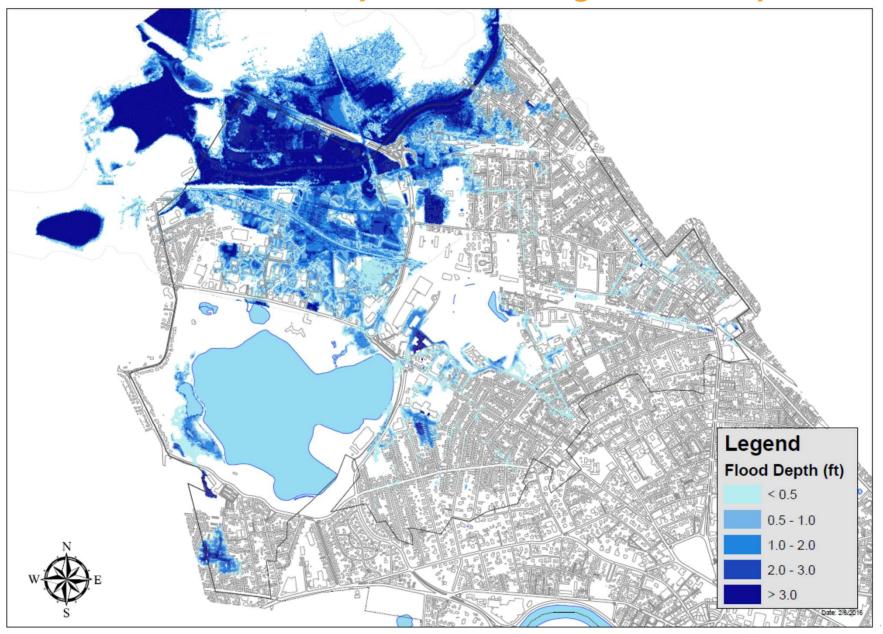
Captured using ADCIRC in the BH-FRM



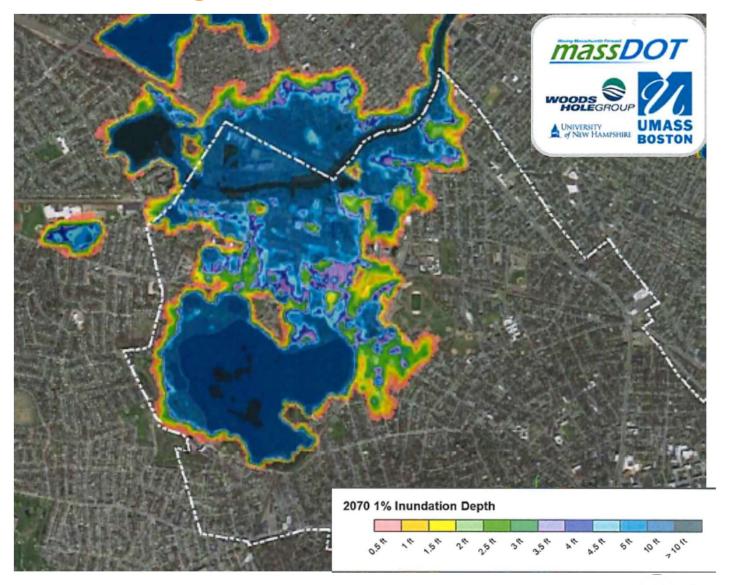
Sewer System Flooding from Precipitation



Riverine and Sewer System Flooding from Precipitation



Riverine Flooding from SLR/SS





CCVA Part 1, Conclusions

Charles River

- Riverine overbank flooding risk is small
- Sewer system flooding is greatly exacerbated
- SLR/SS flooding risk is small and flow pathways are localized

Alewife Brook

- Riverine overbank flooding is significantly increased
- Sewer system flooding is increased
- SLR/SS flood risk and severity are greatly increased by the end of the century

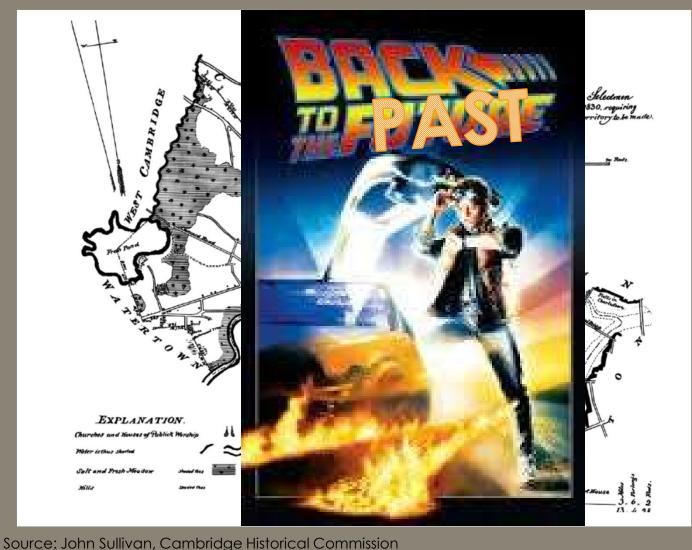


2 The Alewife Brook Area

- This region of Cambridge is the most vulnerable to flooding under climate change
- Flooding risk is augmented by increased precipitation up to midcentury as well as SLR/SS at the end of the century
- The Alewife area will be impacted by both riverine and sewer system flooding



2. The Alewife Brook area in the Future –Title of the Movie?



Stantec

Challenges of a non-integrated approach

- Different flooding types occur at different times
- Flooding is generated by factors of different scale (local or system level for sewer flooding) versus watershed or regional for riverine flooding
- High degree of inter-dependence between systems
- Running scenarios and combinations of scenarios becomes cost and time prohibitive (it's also the worst nightmare for a hydraulic modeler-high chances of error)



3 Hydraulic Modeling Integration

- River Models don't include pipe systems
- Sewer models don't include river systems
- Coastal models don't include pipe systems or hydrology

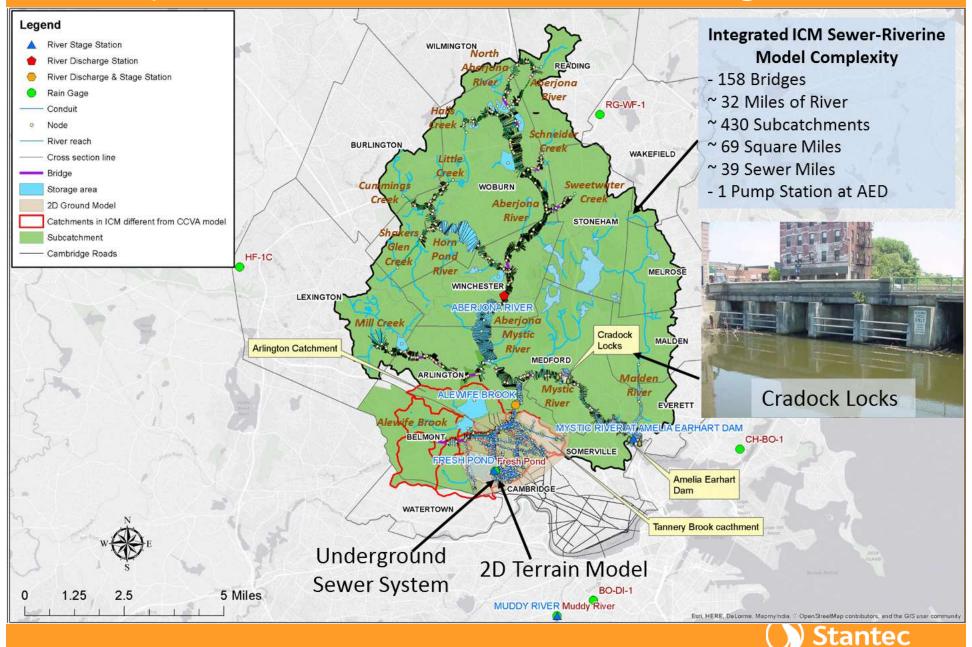


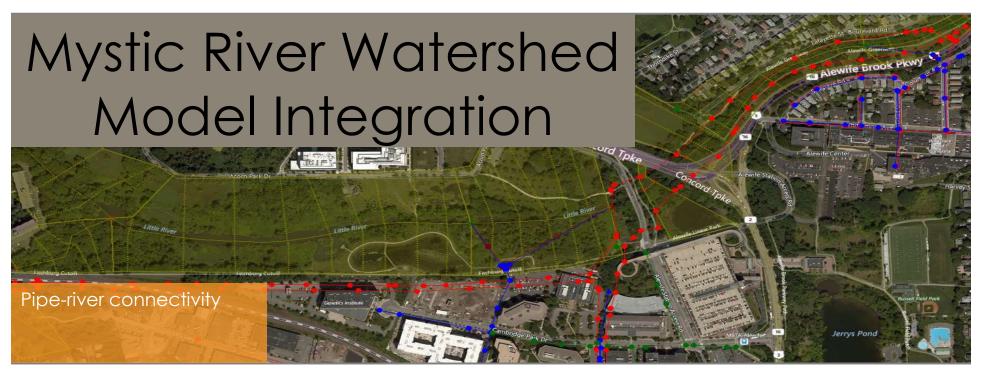
Mystic River Watershed Model Integration

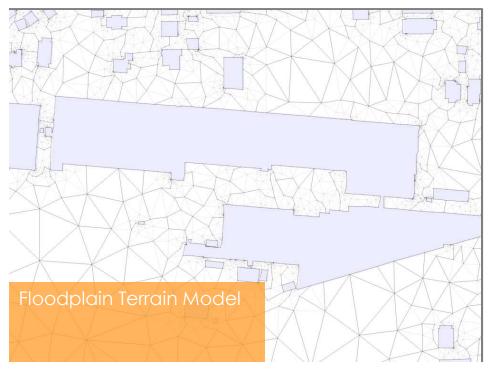
- Watershed scale riverine geometry and hydrologic catchments directly imported from FEMA model used for FIS
- Pipe model was obtained from Cambridge and MWRA regional sewer model
- Both models were integrated seamlessly
- The Cambridge floodplain was generated with a high resolution 2D grid, which includes flow path obstacles
- Operation of the AED was assumed different than FEMA based on communications and calibration

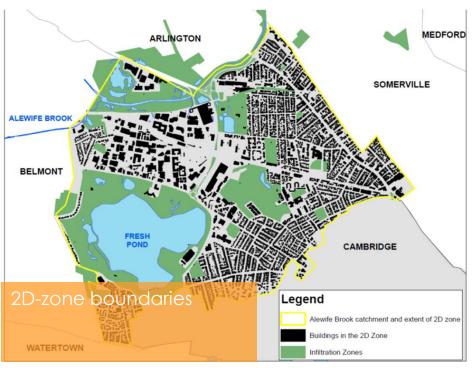


Mystic River Watershed Model Integration









4 Hydraulic Model Calibration and Validation

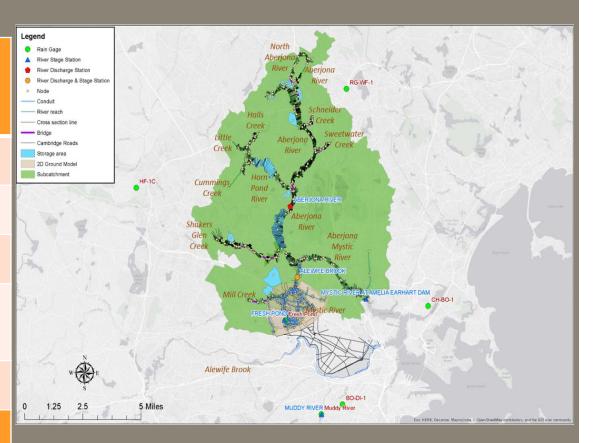


4 Hydraulic Model Calibration and Validation-Selected Storms

	March 2010	May 2006
Start Date/Time	13/8:00	12/17:30
End Date/Time	15/21:00	16/18:30
Total Rainfall (in)	9.59*	7.42*
Peak Intensity (in/hour)	1.32	0.60
Return Period**	>50-yr	~>20-yr

^{*}At Muddy River in Brookline RG

Airport

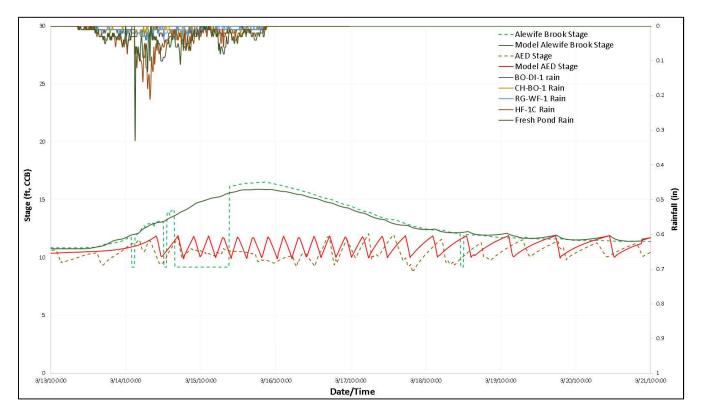




^{**}Based on NOAA Atlas 14 Estimates at Logan

4 Hydraulic Model Calibration - March 2010 River Gages

USGS Station		Model	Meter	Difference (ff)
Alewife Brook	Peak Stage (ft)	15.94	16.52	-0.58
Amelia Earhart Dam	Peak Stage (ft)	11.90	12.05	-0.15





4 Hydraulic Model Calibration - March 2010 River Gages

Comparison between metered and modeled flows for the March 2010 storm event.

USGS Station		Meter	Model	% Difference
Aberjona River	Peak Flow (MGD)	937.16	935.96	-0.1
	Volume (MG)	2957.42	2341.03	-20.8
Alewife Brook	Peak Flow (MGD)	142.72	141.58	-0.8
	Volume (MG)	510.54	532.14	4.2



4 Hydraulic Model Calibration -March 2010 Photographic Evidence



Photographs Courtesy of Cambridge DPW



4 Hydraulic Model Calibration -March 2010 Photographic Evidence

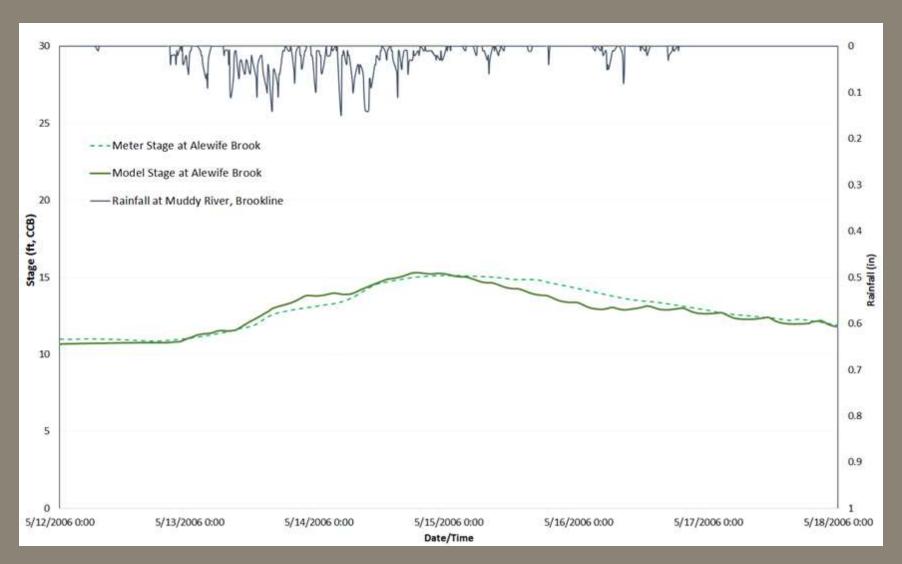






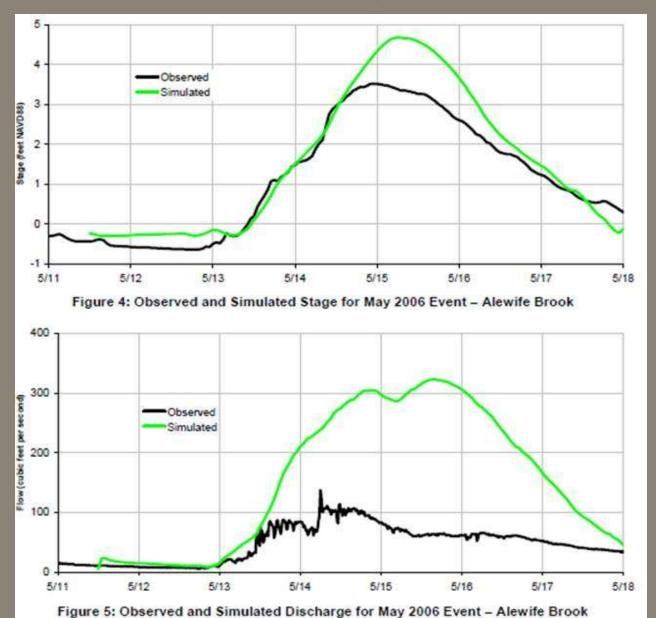


4 Hydraulic Model Validation - Mary 2006





5 Previous Model Calibration





5 Potential Future Uses

- Forecast flood extents during future precipitation-driven scenarios
- Potential to propagate flooding from SLR/SS events
- Potential to asses combinations of precipitation and SLR/SS seamlessly
- Allow for evaluation of mitigation measures at multiple scales alone and in combination



5 List of Potential Local Measures

	Measure	Sewer System Flooding	River Overbank Flooding from Precipitation	River Overbank Flooding from SLR/SSS
Source Controls	Land Use changes		(F)	F
	Peak flow retention		(F)	P
Pathway	Flow Storage		(B)	(F)
Controls	Flow Transfer		()	(F)
	Conveyance Capacity Increase		(F)	P
Receptor Controls	System isolation via berms, walls			

5 List of Potential Watershed Measures

Measure	Sewer System Flooding	River Overbank Flooding from Precipitation	River Overbank Flooding from SLR/SSS
Smart Reservoir Management	(Ja		
Large Scale Land Use Changes			
Removal of Hydraulic Bottlenecks	(B)		
Increase in pumping and sluicing output	P		



5 List of Potential Regional Measures

Measure	Sewer System Flooding	River Overbank Flooding from Precipitation	River Overbank Flooding from SLR/SSS
Topographic changes in flanking paths	()	()	
Revamp of the AED (raising top of the dam)	(F)	(F)	
Flow isolation and real-time flow management	(F)		
Other large scale projects	(F)	Unknown	Unknown



Conclusions

- The model has been successfully integrated, calibrated, and validated
- It will be used to update the CCVA, Part 1 and inform the CCVA CCPR
- The watershed integrated can be refined with more information from watershed communities
- It can be used for watershed and regional decision making and to evaluate effectiveness of those decisions



Thank you!! Questions?

